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DEVELOPMENT OF HIGH STRENGTH STEEL SHEET WITH IMPROVED STRAIN HARDENABILITY FOR AUTOMOTIVE APPLICATION

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Abstract. Advance high strength steel with minimum UTS of 780 MPa is industrially developed utilizing continuous annealing line (CAL) and Gleeble thermo mechanical simulation. An outline of superior elongation, improved strain hardenability, enhanced strength of developed Fe–C–Mn–Si TRIP assisted steel is described. Correlation amid Simulated result and industrially annealed steel are stabilized for microstructure and mechanical property. Annealing condition is optimized for best combination of strength and formability accordingly. CCT diagram for the selected composition from JMatPro is utilized to optimize rapid cooling rate and over aging section temperature. Final microstructure of developed steel comprises tempered martensite, granular bainite with retained austenite distributed in polygonal ferrite matrix. An evaluation of developed TRIP steel is carried out with the help of microstructure and XRD analysis. It was concluded that strain hardening coefficient of new steel is comparable to that of drawing grades attributable to about 13 % retained austenite in microstructure.

Keywords: TRIP steel, retained austenite, continuous annealing, XRD, transformation, automotive steel, heat treatment.

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INTRODUCTION

Lately TRIP assisted steel are in extensive demand for automotive application owing to their excellent strength ductility combination. The concern of strict global environment regulation to reduce tail pipe emission and improved fuel efficiency by BIW weigh reduction has further pushed the use of AHSS steels in automotive [1]. Since TRIP steel offer better combination of enhanced fatigue resistance and drawability, they are considered for novel highly formable cold-rolled steel sheet for automobile body application [2]. The strength deformation combination is attributed to TRIP phenomenon where strain-induced phase transformation of retained austenite (RA) renders excellent strain hardenability (n -value) [3]. While evaluating TRIP assisted steel with Ferrite-Martensite Dual phase grade of same strength, the former shows improved strain hardenability and elongation due to TRIP effect. Additionally, improved formability of

TRIP-steel can be attributed to their composite like deformation behaviour where retained austenite transformation assists in strain distribution in the softer bainite and ferrite constituents [4 – 6]. The improved fatigue life is attributed to relaxation of high stressed field during fatigue by transformation of retained austenite to Martensite [7 – 10]. With said advantages, this study outlines the industrial development of next generation TRIP assisted steel with a tensile strength of atleast 780 MPa.

EXPERIMENTAL

Steel slab of 220 mm thickness with chemical composition (Table 1) as per DIN EN 10338 – HCT780T) grade is industrially produced through basic oxygen furnace (BOF) – RH degasser route in steel melting shop (SMS) and continuously casted subsequently at industrial slab casting machine. Slabs are hot rolled to 2.4 mm at 7-strand hot strip

Table 1

Chemical Composition of HCT780T- TRIP steel

Таблица 1. Химический состав ПНП-стали HCT780T

Grade	C (Max)	Mn (Max)	Si (Max)	P (Max)	S (Max)	Cr + Mo (Max)	Nb + Ti (Max)	V (Max)
HCT780T	0.220	2.000	2.000	0.020	0.005	0.300	0.150	0.050

mill (HSM) keeping the hot finish temperature above A3 and coiling in the range from 550 – 600 °C. Acid pickling and cold rolling (1.2 mm) is carried out at pickling line tandem with cold rolling mill (PLTCM). Cold rolled samples are simulated at Gleeble 3800 thermo mechanical simulator and processed at industrial Continuous annealing line (CAL) respectively. JMatPro simulation software is utilized to generate composition based CCT curves. Tensile tests are carried out as per ISO 6892-1:2009(E) standard in Zwick Roell-100KN tensile testing machine. Microstructure examination is carried in Carl Zeiss Optical microscope at and Hitachi Scanning Electron microscope utilizing SE mode. XRD analysis is done at PANalytical – Empyrean X-ray diffractometer with Cu-K α Source.

RESULT AND DISCUSSIONS

Hot Rolled and Cold Rolled Microstructure and Properties

As given in Fig. 1a, Ferrite-pearlite microstructure at hot rolled (HR) stage is broken down to elongated ferrite and pearlite microstructure with small precipitates of cementite (Fig 1b.) post 50 % cold rolling. Pearlitic microstructure at HR stage is due to high coiling temperature (>550 °C) during hot rolling which is above the bainite start temperature as given in CCT diagram of sleeted steel composition.

CCT Curve and Annealing cycle

Fig. 2a and Fig. 2b demonstrate TTT and CCT curves respectively acquired from JMatPro Thermo-Physical simulation software to calculate various critical temperature for given TRIP steel composition. As seen in Fig. 2a and Fig. 2b, Bainite start temperature (B_s) is close to 480 °C where as M_s temperature is close to 380 °C. Based on the CCT curve, Gleeble and in line CAL trials are carried out to optimize the annealing condition for better strength – ductility combination. Fig. 3 depicts typical CAL/Gleeble annealing cycle with different over aging temperature tryouts for Cold rolled Closed Annealed (CRCA) steel sheet.

Microstructure Post Continuous Annealing

Typical mechanical property of Continuous Annealed and Gleeble simulated samples are listed in Table 3. As given in Table 3, excellent combination if Strength (UTS > 850 MPa) with superior elongation and strain hardenability could be achieved post annealing. Annealing with Soaking temperature of 800 °C with cooling rate <25 °C/s and over aging temperature of 450 °C lead to above listed mechanical properties.

Fig. 4a and Fig. 4b shows the SEM and Optical micrograph of CAL annealed sample annealed at A3–20 °C. Rapid cooling end and Overaging section temperatures

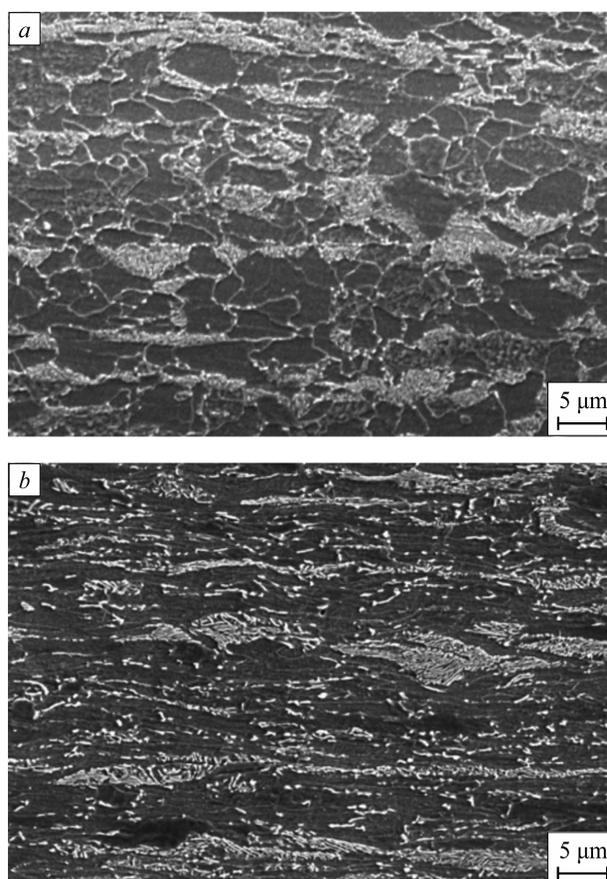


Fig. 1. SEM Micrograph of TRIP Steel, $\times 2000$:
a – hot-rolled; b – cold rolled

Рис. 1. СЭМ-микрoграфия ПНП-стали, $\times 2000$:
a – горячекатаная; b – холоднокатаная

Table 2

Mechanical properties Hot rolled and Cold Rolled Samples HCT780T steel

Таблица 2. Механические свойства горяче- и холоднокатаных образцов стали HCT780T

Grade	YS (MPa)	UTS(MPa)	El %, 50 gl
Hot Rolled	660 \pm 15	778 \pm 12	18 \pm 1
Cold Rolled (Full Hard)	1050 \pm 10	1170 \pm 15	5 \pm 1

are kept at B_s –40 °C and B_s –30 °C respectively, where as B_s is Bainite start temperature for given composition calculated from JmatPro. Optical micrograph shows island of Bainite, Retained Austenite (RA) along with small fraction of Martensite (M) distributed in Recrystallized ferrite matrix. Fig. 4c shows distribution of different microstructural constituents where Ferrite is shown as Green, Bainite as Blue and Retained Austenite/Martensite as brown color. XRD diffraction pattern given in Fig. 4d suggested about 13 % of RA in the microstructure where as 25 % Bainite and 55 % Ferrite are calculated from Optical micrograph. Martensite fraction (~7 %) is calculated from deducting

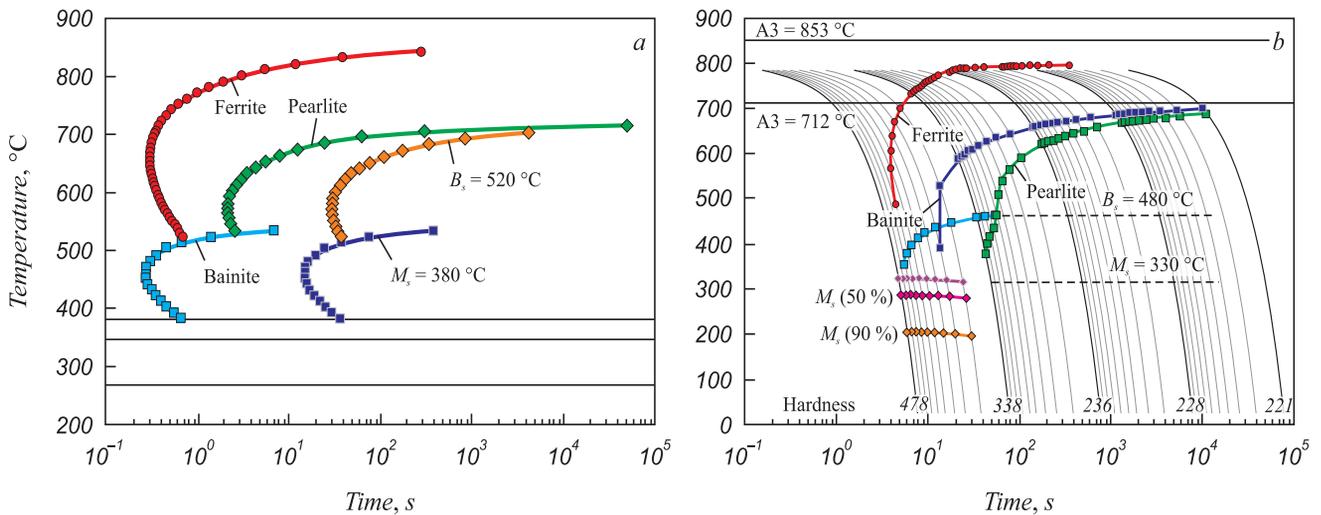


Fig. 2. TRIP Steel of selected Composition:
a – TTT diagram; b – CCT diagram

Рис. 2. ПНП-сталь выбранного состава:
a – диаграмма время–температура–выделение; b – термокинетическая диаграмма

RA fraction from RA + M fraction which is about 20 % for given sample.

Annealing Parameters vs. Mechanical Properties

Cold rolled coils and full hard samples are processed at CAL and Gleeble Thermo mechanical simulator respectively at different Soaking (Annealing) and Overaging Temperatures. Mechanical properties are evaluated for optimum strength–ductility balance. Soaking temperature (SS) is varied from $A3-100\text{ }^{\circ}\text{C}$ to $A3+10\text{ }^{\circ}\text{C}$, where A3 is upper critical temperature calculated in JMatPro. To study the effect of soaking temperature, rapid cooling (RCS) and Overaging (OAS) temperatures were kept constant as $B_s-40\text{ }^{\circ}\text{C}$ and $B_s-30\text{ }^{\circ}\text{C}$ respectively. As evident from Fig. 5a, superior strength and elongation combination can be achieved at soaking temperature of $A3-20\text{ }^{\circ}\text{C}$ having UTS of atleast 850 MPa and Elongation more than 25 %. It is also observed that increasing SS over A3 doesn't have

any significant impact on strength or elongation as keeping soaking temperature above A3 result in larger austenite grain size degrading the final strength. Keeping SS to $A3-100\text{ }^{\circ}\text{C}$ (Fig. 5a) resulted in poor elongation as at such a low temperature of intercritical annealing, the amount of retained austenite in final microstructure is not sufficient to give sufficient TRIP effect.

To analyze the impact of Overaging temperature as given in typical annealing cycle (Fig. 3), OAS in CAL is varied from B_s-130 to $B_s+140\text{ }^{\circ}\text{C}$ while keeping the Soaking temperature constant at $A3-20\text{ }^{\circ}\text{C}$. Similar cycle is simulated in Gleeble as well. Rapid cooling end temperature is always kept OAS+10 °C for each trial. As evident from Fig. 6b an optimum combination of Strength (855 MPa), Elongation (25 %) and excellent strain hardenability (*n*-value) of 0.22 is achieved at OAS temperature of $B_s-40\text{ }^{\circ}\text{C}$ at CAL. The result is attributed to 13 % RA along with 55 % ferrite and 25 % Bainite in microstructure (Fig. 4b to Fig. 4d). Keeping OAS temperature down to $B_s-130\text{ }^{\circ}\text{C}$ (Fig. 6a) results in elevated strength of 903 MPa due to increased Martensite phase fraction; however the resultant elongation drops significantly due to lower retained austenite (<2 %) in microstructure.

Table 3

Typical Mechanical properties of Trip 780 steel post Annealing

Таблица 3. Стандартные механические свойства ПНП-стали 780 после отжига

Grade	YS (MPa)	UTS (MPa)	El%,50 gl	<i>n</i> -value
CAL	480 ± 9	854 ± 12	25.0 ± 1.0	0.23 ± 0.01
Gleeble	468 ± 13	843 ± 15	24.5 ± 1.5	0.22 ± 0.01

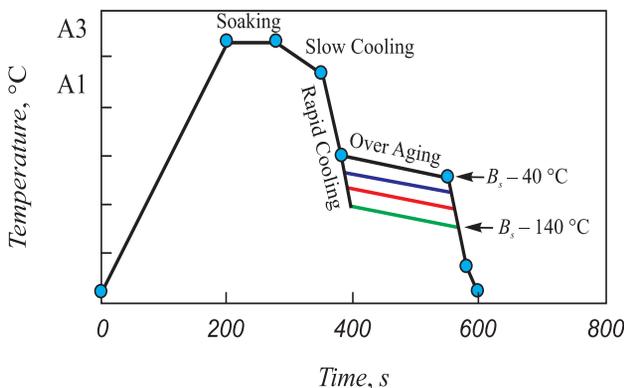


Fig. 3. Typical CAL annealing Cycle

Рис. 3. Стандартная схема отжига на ЛНО

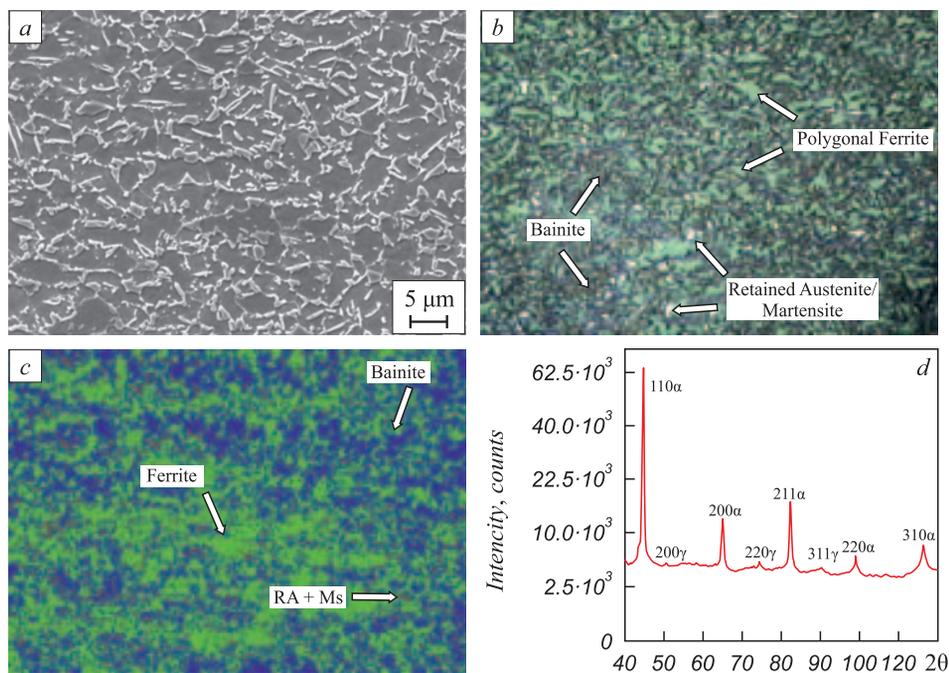


Fig. 4. Continuous annealed microstructures of 780 TRIP steel:
 a – SEM micrograph; b – optical micrograph; c – color map of distribution of different phases; d – XRD diffraction pattern

Рис. 4. Непрерывно-отожженные микроструктуры ПНП-стали 780:
 a – СЭМ-микротография; b – оптическая микротография; c – цветная карта распределения разных фаз;
 d – дифракционная рентгенограмма

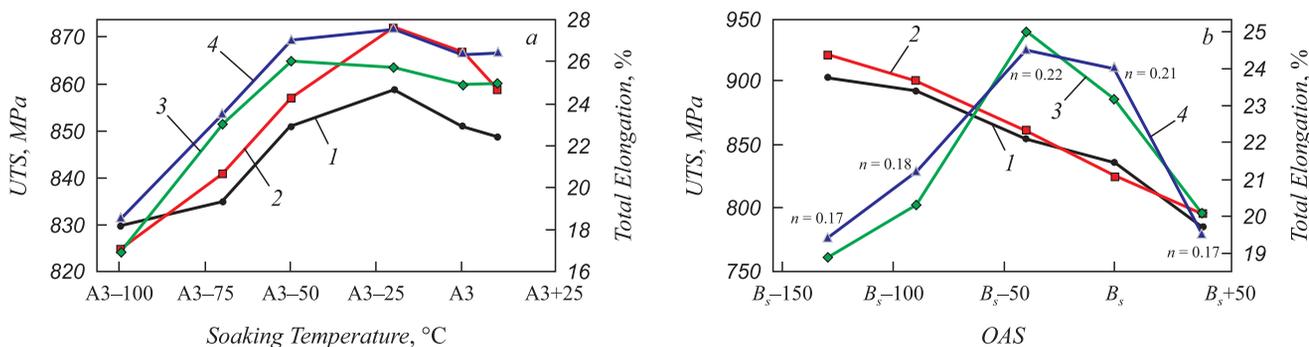


Fig. 5. Dependences for CAL and Gleeble Simulation:
 a – soaking temperature vs. UTS/EI %; b – overaging section temperature vs. UTS/EI %;
 1 – UTS – CAL; 2 – UTS – Gleeble; 3 – EI % – CAL; 4 – EI % – Gleeble

Рис. 5. Зависимости для моделирования ЛНО и Gleeble:
 a – температуры выдержки от предела прочности на разрыв/EI %; b – температуры старения секции от предела прочности на разрыв/EI %;
 1 – UTS – CAL; 2 – UTS – Gleeble; 3 – EI % – CAL; 4 – EI % – Gleeble

CONCLUSION

With selective combination of chemical composition and annealing parameters, HCT 780T Trip steel has been successfully developed industrially and validated through Gleeble simulation. Resultant steel confirm improved strength–drawability combination with excellent strain hardenability. It is also concluded that Keeping SS temperature of A3–30 °C and OAS temperature of B_s –40 °C gives optimum result with 13 % retained austenite for given composition. However, keeping OAS at reduced level of

B_s –140 °C and Soaking A3–100 °C resulted in poor elongation.

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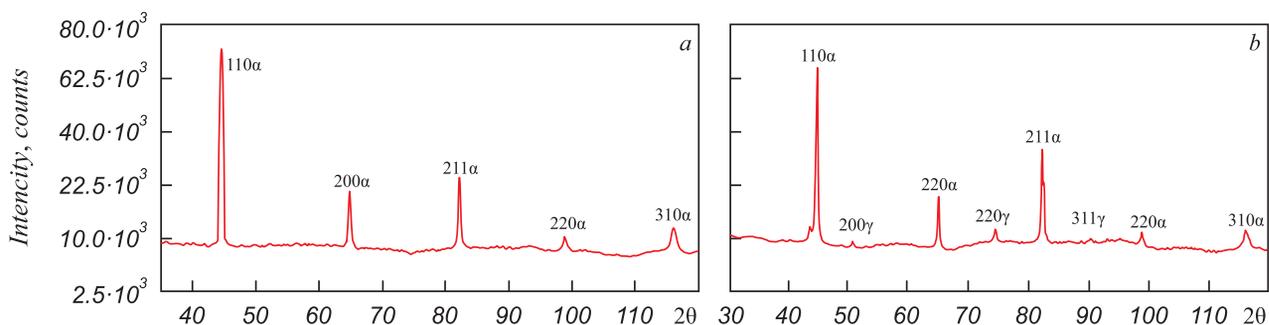


Fig. 6. XRD pattern of the sample processed at:
 a – OAS B_s – 140 °C; b – OAS B_s – 40 °C

Рис. 6. Рентгенограмма образца после выдержки в масле при:
 a – 140 °C; b – 40 °C

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РАЗРАБОТКА ВЫСОКОПРОЧНОГО СТАЛЬНОГО ЛИСТА С УЛУЧШЕННОЙ ДЕФОРМАЦИОННОЙ ПРОКАЛИВАЕМОСТЬЮ ДЛЯ АВТОМОБИЛЬНОЙ ПРОМЫШЛЕННОСТИ

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Аннотация. Передовая высокопрочная сталь с минимальным пределом прочности на разрыв 780 МПа была разработана промышленным способом с использованием линии непрерывного отжига (ЛНО) и термомеханического моделирования Gleeble. Разработанная Fe–C–Mn–Si ПНП-сталь обладает повышенной деформационной прокаливаемостью, прочностью и относительным удлинением. Корреляция между моделируемым результатом и промышленно отожженной сталью видна по микроструктуре и механическим свойствам. Условия отжига оптимизированы для наилучшего сочетания прочности и формовости. Термокинетическая диаграмма для выбранной JMatPro композиции используется для оптимизации скорости охлаждения и температурных режимов старения. Конечная микроструктура разработанной стали состоит из закаленного мартенсита и сфероидизированного бейнита с остаточным аустенитом, распределенным в полигональной ферритовой матрице. Оценка разработанной ПНП-стали проводилась с помощью оптического и рентгеноструктурного анализа. В результате ис-

следований установлено, что коэффициент деформационного упрочнения новой стали сравним с коэффициентом упрочнения марок, содержащих приблизительно 13 % остаточного аустенита в микроструктуре.

Ключевые слова: ПНП-сталь, остаточный аустенит, непрерывный отжиг, рентгеноструктурный анализ, трансформация, автомобильная сталь, термообработка.

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